

A 1V 11fJ/Conversion-Step 10bit 10MS/s Asynchronous SAR ADC in 0.18μm CMOS

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Abstract

This paper presents a 10-bit SAR ADC using a variable window function to reduce the unnecessary switching in DAC network. At 10-MS/s and 1-V supply, the ADC consumes only 98 μW and achieves an SNDR of 60.97 dB, resulting in an FOM of 11 fJ/Conversion-step. The prototype is fabricated in a 0.18μm CMOS technology.

Introduction

The DAC switching network in [1] saves 81% switching energy and 50% total capacitance as compared to the conventional one. However, the signal-dependent comparator offset caused by the input common-mode voltage variation degrades the ADC performance. Hence, this paper presents a splitting monotonic switching procedure to maintain the common-mode voltage during bit cycling.

Besides, the conventional SAR ADCs apply a binary search algorithm to approach the closest digital code to match the input signal. In a typical conversion, the reference DAC is added or subtracted a binary-weighted voltage according to the comparator output in each bit cycles. In the last cycle, the difference between input signal and reference is less than one LSB. However, during the conversion, the difference increases when adds a large voltage to a small difference, that results in unnecessary energy wasted. Fig. 1 shows the concept of our idea. When the difference is small, this ADC does not add or subtract any voltages until the remaining bit cycling operations could not reduce the difference to less one LSB. A variable window function is presented to ensure the difference does not increase during the conversion. The multi-comparator SAR ADCs [2-3] are able to reduce the risk of metastability and power consumption in comparators. This work uses the multi-comparator concept to perform the variable window function to reduce the unnecessary switching in DAC network. The method saves the power consumption in comparators, capacitor networks and switch buffers at the expense of little hardware overhead.

Circuit Description

Fig. 2 shows the schematic of the proposed SAR ADC. Similar to the split capacitor array [4], the first 4 MSB capacitors in the capacitor array are all split into two equal sub-capacitors to perform the splitting monotonic switching method. At the sampling phase, the top plates of all capacitors capture the input signal via the bootstrapped switches. At the

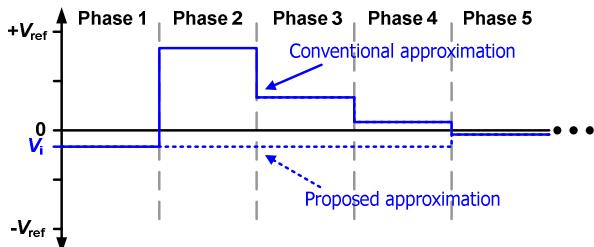


Fig. 1: The approximations of conventional and proposed methods.

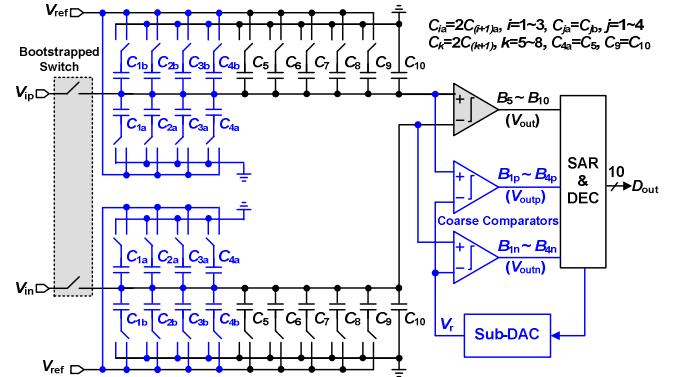


Fig. 2: The proposed SAR ADC.

same time, the bottom plates of capacitors $C_{1a} \sim C_{4a}$ are reset to ground, and the others ($C_{1b} \sim C_{4b}$ and $C_5 \sim C_9$) are reset to V_{ref} . Next, the comparators do the first comparison. The capacitor C_{1b} on the higher voltage potential side is pulled down to ground. On the lower voltage potential side, the capacitor C_{1a} is pulled up to V_{ref} . Therefore, the common-mode voltage does not change. To avoid complicated control logic and layout routing, the splitting monotonic switching method is only applied to the first 4 MSB capacitors. The remaining operations still use the switching method in [1]. The common-mode voltage variation is diminished to only 1/16 of that in [1]. The comparator dynamic offset problem becomes negligible in this 10-bit case.

Fig. 3 shows how to reduce the unnecessary switching in DAC network. Take the Phase 1 as an example. When the voltage difference of input signal and reference is located in the “No Switching” region, even no capacitors switched in this cycle, the remaining bit cycling operations could reduce the difference to less than one LSB. Hence, this ADC does not switch any capacitors in this bit cycle. On the contrary, when the voltage difference is located in the “Switching” region, this ADC switches the relative capacitors according to the comparison. Otherwise the remaining bit cycling operations could not reduce the difference to less than one LSB.

Two coarse comparators and a sub-DAC are added to perform the function as shown in Fig. 3. In order to achieve a variable window function in different bit cycles, the reference voltage V_r must be variable. Fig. 4 shows the variable window

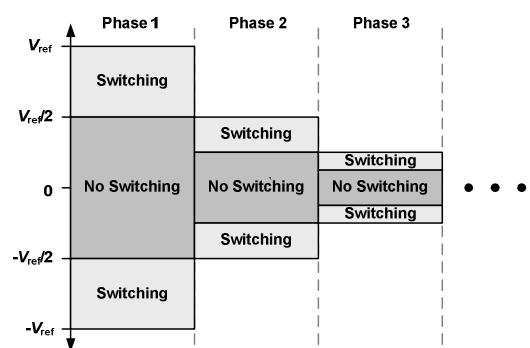


Fig. 3: The graph of proposed switching procedure.

function and V_r . A 6-bit sub-DAC generates the variable V_r . The real V_r in this ADC is large than the ideal value about 8 LSB, the real window size is a little smaller than the ideal one. Therefore, this ADC has about 8 LSB margin to tolerance the sub-DAC and coarse comparator offset errors. For best efficiency, the mechanism only used in first 4 MSB capacitors. Even includes the overhead of the 6-bit sub-DAC, this method saves 40~45% power dissipation in the capacitor network and switch buffers compared to [1]. Fig. 5 shows the digital error correction logic, which consists of only 4 full-adders.

This ADC uses a dynamic comparator with a p-type input pair. The dynamic comparator does not consume static current and hence is suitable for an energy efficient design. Internal control logic triggered by the global clock and comparator output asynchronously generates internal control clocks, which avoids a high frequency clock generator and makes the sampling rate equal to the clock rate. This ADC uses metal-oxide-metal (MOM) capacitors to construct the capacitor array. The unit capacitor is about 5 fF, composed of 5 metal layers in a $4 \times 4.8 \mu\text{m}^2$ area. The total input capacitance is 2.5 pF each terminal. According to simulation result, this ADC saves about 17.6 % power consumption than the architecture in [1]. Besides, with less capacitors switched, the DNL and INL performance was improved especially around the middle of output codes. Hence, the linearity of ADC is enhanced.

Experimental Result

The prototype is fabricated in a $0.18\text{-}\mu\text{m}$ CMOS technology. The micrograph is shown in Fig. 6. The active core area is only $330 \times 260 \mu\text{m}^2$. At 10-MS/s, 1-V supply and 1-MHz input stimulus, the measured static performances are plotted in Fig. 7. The peak DNL and INL are +0.28/-0.34 LSB and +0.23/-0.38 LSB, respectively. The measured SNDR and SFDR are 60.97 and 79.4 dB, respectively. The resultant ENOB is 9.83 bit. Fig. 8 plots the measured SFDR and SNDR versus input frequency and FFT spectrum with input frequency closes to Nyquist frequency. The analog circuit, including the S/H circuit and comparators, consumes 32 μW , and the digital control circuit draws 50 μW . The capacitor networks and Sub-DAC consume 16 μW . The total power consumption of the ADC is 98 μW . The prototype achieves an FOM of only 11 fJ/conversion-step. Table I summarizes the comparison to state-of-the-art ADCs.

Acknowledgement

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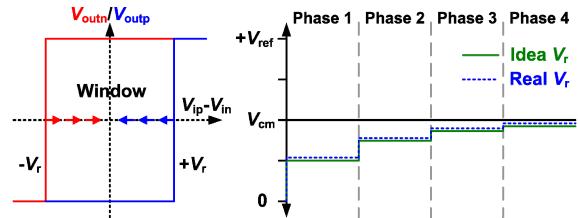


Fig. 4: Variable window function.

	B_{xp}	B_{xm}	State
$V_{ip} > V_r$	1	1	Switching
$V_{in} < V_r$	1	0	No Switching
$V_{ip} < V_r$	0	0	Switching

Fig. 5: Digital error correction logic.

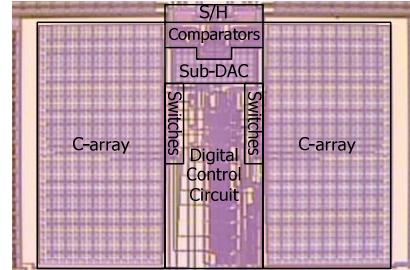


Fig. 6: Chip micrograph.

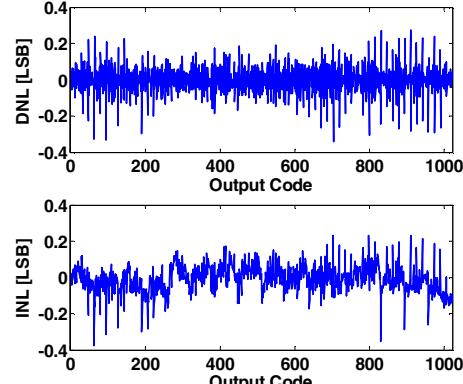


Fig. 7: Measured DNL and INL.

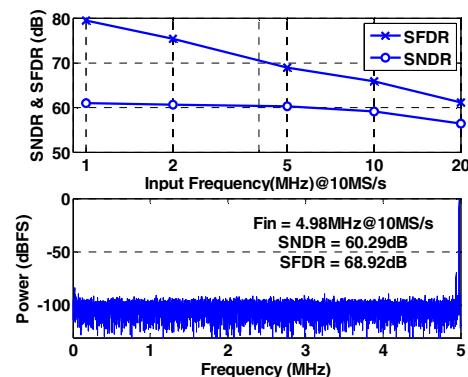


Fig. 8: Measured dynamic performance

Table I. Comparison to state-of-the-art works

Specification (Unit)	[1]	[2]	[3]	This work
Technology	$0.13\mu\text{m}$	$0.13\mu\text{m}$	$0.18\mu\text{m}$	$0.18\mu\text{m}$
Supply Voltage (V)	1.2	1	1	1
Resolution (bit)	10	12	10	10
Sampling rate (MHz)	50	11	0.5	10
ENOB (bit)	8.48	10.1	9.4	9.83
Power (μW)	920	3570	42	98
FOM (fJ/Conv.-Step)	52	311	124	11
Active area (mm^2)	0.075	0.7	0.24	0.086